

An Improved Scheme Asymmetrically and Symmetrically Clipped DC-Biased Optical (ASDCO)-OFDM for Wireless IM/DD Optical System

Bipul Kumar Singh Deo

Gautam Buddha University
Greater Noida
vipulsingh369@gmail.com

Abhilash Singh

Gautam Buddha University
Greater Noida
abhilash12iec002@gmail.com

Rahul Kumar

Gautam Buddha University
Greater noida
rahulupadhyay2k16@gmail.com

Pradeep Bhardwaj

G L Bajaj Centre for Research and
Development
GLBITM, G.Noida, India
pradeep.bhardwaj@glbitm.org

Krishna Kant Singh

G L Bajaj Centre for Research and
Development
GLBITM, G.Noida, India
krishnaiitr2011@gmail.com

ShashankTripathi

G L Bajaj Centre for Research and
Development
GLBITM, G.Noida, India
shashanktripathi030@gmail.com

Abstract—In this paper, a modified system built on (ASCO)-OFDM, that can be utilized in IM/DD wireless optical system is designed and analyzed. At the transmitter the modified ASDCO-OFDM scheme uses the fact of nullifying the mean dc-bias of subcarriers generated after the Hermitian symmetry and removal of interference at the receiver with the help of equalizer. By utilizing this modified scheme both odd and even subcarriers are modulated to convey the input signal. The modulations of subcarriers that are odd are performed by ACO-OFDM whereas modulations of subcarriers that are even are performed by SCO-OFDM which is a novel modulation scheme. ACO-OFDM and SCO-OFDM causes asymmetrically clipping noise and symmetrically clipping noise in the generated system. These interferences can be assessed and expelled at the receiver using zero forcing equalizer. Therefore, this scheme helps in accomplishing superior efficiency in terms of Symbol Error Rate(SER) and Optical power as compared to ASCO-OFDM.

Keywords—ASCO-OFDM; ASDCO-OFDM; IM/DD; SER; Optical power.

I. INTRODUCTION

Optical wireless systems with intensity modulation direct detection (IM/DD) can be efficient substitute to wireless systems. Radio Frequencies (RF) are used for transmission of data at high speed in an indoor environment. They are the most widely studied areas in current scenario [1-3]. Optical Wireless Communication (OWC) in comparison to RF communication offers inexhaustible transmission bandwidth. An economical spatial diversity is reached with a large space detector and short carrier wavelengths [4]. Multipath distortion occurs that is brought on by reflection from dividers or household items, which sorely disturbs the characteristics of transmission of an optical signal.

In RF communication, to battle inter-symbol interference (ISI) caused by multipath propagation, a promising modulation technique that has been widely adapted is commonly known as Orthogonal Frequency Division Multiplexing (OFDM) [5]. An asymmetrically clipped optical OFDM (ACO-OFDM) [6,7] and DC-biased optical OFDM (DCO-OFDM) [8] are the two different techniques of OFDM that have been effectively utilized in IM/DD OWC. An asymmetrically clipped DC-biased optical OFDM (ADO-OFDM) [9] has been built up in conjunction with the methods of the aforementioned procedures and it is a lot economical in case of optical power and bandwidth. Additionally, polar-OFDM and a hybrid model of ACO-OFDM are the perfect examples of OFDM systems that are spectrally economical [10,11].

The information carrying data stream is allowed to be modulated into the intensity of optical carriers, in optical wireless systems. Thus, to perceive the intensity modulation solely real and positive values may be used. With a specific end goal to achieve a signal that is real and to translate blocks of Hermitian symmetry complex symbols an Inverse Fast Fourier Transform (IFFT) must be applied. Two conventional techniques that are adopted in a large extent, for the positive demand of the transmitted optical signals are clipping and addition of DC bias. In DCO-OFDM, to abolish the non-positive values we have to add some DC bias within the transmitted signal. However, the DC bias level strongly ensures the performance of DCO-OFDM [12]. The negative values which are left should be fixed to zero, if the negative peak is not exceeded by the added DC bias, then all subcarriers are plagued by noise caused due to clipping. The DCO-OFDM in the case of optical power becomes inefficient, if the negative peak is smaller than the DC bias. DCO-OFDM is bandwidth efficient in light of the fact that even subcarriers as

well as odd subcarriers are utilized to convey information. In ACO-OFDM, only positive values will remain as all the non-positive values are fixed to zero. In [13], it is given that on the even subcarriers all the clipping noise falls without manipulating the information on the subcarriers and it does not affect the data of the odd subcarriers. This reduces the amplitude of the actual symbols to half by applying the clipping approach. Thus, to carry information in ACO-OFDM solely odd subcarriers are used. ACO-OFDM is efficient in case of optical power compared to DCO-OFDM, but its information measure is double that of DCO-OFDM. A grouping scheme known as ADO-OFDM has been created, to maintain the benefits and avoid shortcomings of the aforementioned optical systems. In general, the even and the odd subcarriers are modulated by DCO-OFDM and ACO-OFDM symbols respectively. ACO-OFDM and DCO-OFDM produce some non-positive values which are discretely clipped to zero. Then, by using a LED [14,15] the totality of the two left over positive signals is communicated. By sensing the information conveyed with the help of odd subcarriers, ACO-OFDM symbols can be effortlessly recuperated. On receiving the ACO-OFDM signal one can easily predict the ACO-OFDM clipping noise at the transmitter end by adding a reasonable DC bias. An insignificant clipping noise is produced related to the desired signal by DCO-OFDM. Finally, the symbols of DCO-OFDM are magnificently regained by deducting the expected clipping noise of ACO-OFDM signal from the obtained DCO-OFDM signals.

A modest and straight methodology is the addition of DC bias at the transmitter, however it ends up in a huge left-over of optical power [11]. A hybrid ACO-OFDM which is completely spectrally competent optical system has been proposed by M. Kavehrad and B. Ranjha. Hybrid ACO-OFDM is more power efficient than ADO-OFDM, even when deprived of using the DC bias. Our suggested system and the model of the hybrid ACO-OFDM follow similar concepts. ACO-OFDM symbols are being carried by the odd subcarriers used for the hybrid ACO-OFDM and also for our suggested system. The dissimilarities are that even subcarriers are mapped to the QAM symbols while in event of the hybrid ACO-OFDM to transmit PAM-DMT symbols it makes use of the even subcarriers imaginary parts. We have certainty that our suggested model will be superior to the hybrid model of ACO-OFDM due to the fact that the PAM symbols are much greater than the average power of QAM symbols within the same level of constellation case.

Until now, for attaining real signals the restriction of Hermitian symmetry is generally imposed on the signal vector. Though, to produce real unipolar signals without the restriction of Hermitian symmetry alternative scheme was provided also known as polar-OFDM (P-OFDM) by T.D.C. Little and H. Elgala. The QAM symbols are mapped only to the even subcarriers. The half wave even symmetry is obtained by the signal vectors that are complex after the IFFT operation. At that point, to obtain exponential signal from the

complex form the authors applied the Cartesian-polar operation [11]. The phase values and amplitude of different samples are communicated. The reverse operation is used by T.D.C. Little and H. Elgala to recuperate the initial complex symbols at the receiver end. There are some differences in the designing concepts of our anticipated system and P-OFDM. The use of Hermitian symmetry restriction plays a vital role. Authors have used more DC-bias in the configuration of aforementioned techniques which leads huge wastage of optical power. The ASDCO-OFDM construction details are given in section III.

In this paper, we have used a different methodology, which is an improved version of ASCO-OFDM [16]. This modified ASDCO scheme uses the fact of nullifying the mean dc-bias of subcarriers generated after the Hermitian symmetry. At the same time we are using even subcarriers to transmit (SCO)-OFDM symbols and odd subcarriers to transmit symbols of (ACO)-OFDM. ACO-OFDM symbol fulfills this condition of $x(n) = -x(n+N)$ that comprises of odd subcarriers [13,17] and $x(n) = x(n+N)$ for symbol which is regenerated solely from the subcarriers that are even, if we assume the signal length to be $2N$. In the first and second half subsequent to clipping, similar non-positive values are eliminated. Therefore the positive signals are referred to as symmetrical clipping optical-OFDM signals. Since the ACO-OFDM symbols fall on top of the even subcarriers, they are not influenced by the clipping noise of the SCO-OFDM. By utilizing a similar process in ADO-OFDM, we can retrieve symbols of ACO-OFDM by bringing out the information on the odd subcarriers. Similarly, the clipping noise of ACO-OFDM can be precisely assessed from the recuperated ACO-OFDM signals. The clipping noise of the ACO-OFDM, the SCO-OFDM, and the various noises bring about the contortion of data on the even subcarriers. In section II we examine the subtle elements of reproducing SCO-OFDM. In terms of symbol error rate (SER) and also optical power, this methodology of ours unveils superior performances, as there is absence of DC bias from all subcarriers. In addition, to boost the SER execution [18] the existing method [19] can be applied.

This paper is sorted as follows: Apart from the section I, in Section II A, the arrangement of ASCO-OFDM is quickly looked into. In Section II B, we introduce the improved ASDCO-OFDM framework in detail. In Section III the examination of power/bit and the average Bitrate/Normalized Bandwidths for ASDCO-OFDM and ASCO-OFDM is introduced. Performance evaluations and simulation outcomes between ASCO-OFDM and improved ASDCO-OFDM are given in Section IV. Lastly, the conclusion of the work in Section V.

II. SYSTEM MODEL

A. Survey of asymmetrically and symmetrically clipping optical(ASCO)-OFDM

The ASCO-OFDM's block diagram is displayed in Fig 1.(ASCO)-OFDM system input is a block which is separated into 3 parts out of which two of the signal vectors are of lengths $(N/2) \times 1$ and $(N/2 - 1) \times 1$ respectively. Thus total number of complex data symbols are of length $(3N/2 - 1) \times 1$. Likewise, we have to form the IFFTs input to satisfy the Hermitian symmetry, so as to get a real signal. To form X_{odd}^i and X_{odd}^j signal vectors of length $2N \times 1$, two signal vectors of length $(N/2 \times 1)$ are united with signal vectors which are conjugate to them in series and in the even subcarriers we inject some zeroes, which are given by:

$$X_{odd}^i = \left[0, S_0^i, 0, S_1^i, 0, \dots, 0, S_{\frac{N}{2}}^i, 0, S_{\frac{N}{2}}^{i*}, 0, \dots, S_1^{i*}, 0, S_0^i \right]^T \quad (1)$$

$$X_{odd}^j = \left[0, S_0^j, 0, S_1^j, 0, \dots, 0, S_{\frac{N}{2}}^j, 0, S_{\frac{N}{2}}^{j*}, 0, \dots, S_1^{j*}, 0, S_0^j \right]^T \quad (2)$$

The X_{even} signal vector of length $(N/2 - 1) \times 1$ is characterized correspondingly with zeroes embedded in the subcarriers that are odd to frame the signal in this way:

$$X_{even} = \left[0, 0, S_0, 0, S_1, \dots, S_{\frac{N}{2}-1}, 0, 0, 0, S_{\frac{N}{2}-1}, \dots, S_1, 0, S_0, 0 \right]^T \quad (3)$$

Hermitian symmetry is the important constraint for X_{odd}^i, X_{odd}^j and X_{even} signal vectors. In order to yield signal vectors x_{odd}^j, x_{odd}^i and x_{even} that are real bipolar, both X_{odd}^i and X_{even} are subjected to $2N$ point Inverse Fast Fourier Transform. Zero clipping operation is performed for the non-positive values in x_{odd}^j and x_{odd}^i to produce $x_{odd}^{j,c}$ and $x_{odd}^{i,c}$ respectively. The non-positive values in the x_{even} and the positive values in the x_{even} are clipped to attain a value of zero to yield x_{even}^{cn} and x_{even}^{cp} . To transmit these clipped signals we add $x_{odd}^{j,c}$ with x_{even}^{cp} and $x_{odd}^{i,c}$ with x_{even}^{cn} and then we concatenate these two blocks of signal matrix one after the other. x_{ASCO}^{ij} is the signal that's need to be transmitted which is the sum of cyclic prefix (CP) and these clipped signal.

A multipath propagation channel can also be used to model an indoor optical wireless channel [20]. Optical channel's impulse response is specified by $c(n) = [c(0), c(1), \dots, c(l)]$, cyclic prefix's length is decided by the amount of channel coefficients and is depicted by l . The received optical signal's intensity is sensed by an active photodiode at the receiver the optical channels convolution with the optical signal plus some noise gives $y_{ASCO}^{ij}(n)$:

$$y_{ASCO}^{ij}(n) = w(n) + h(n) \otimes x_{ASCO}^{ij}(n) \quad (4)$$

Thermal noise with the combination of shot noise is represented by $w(n)$. This combination can also be estimated as AWGN.

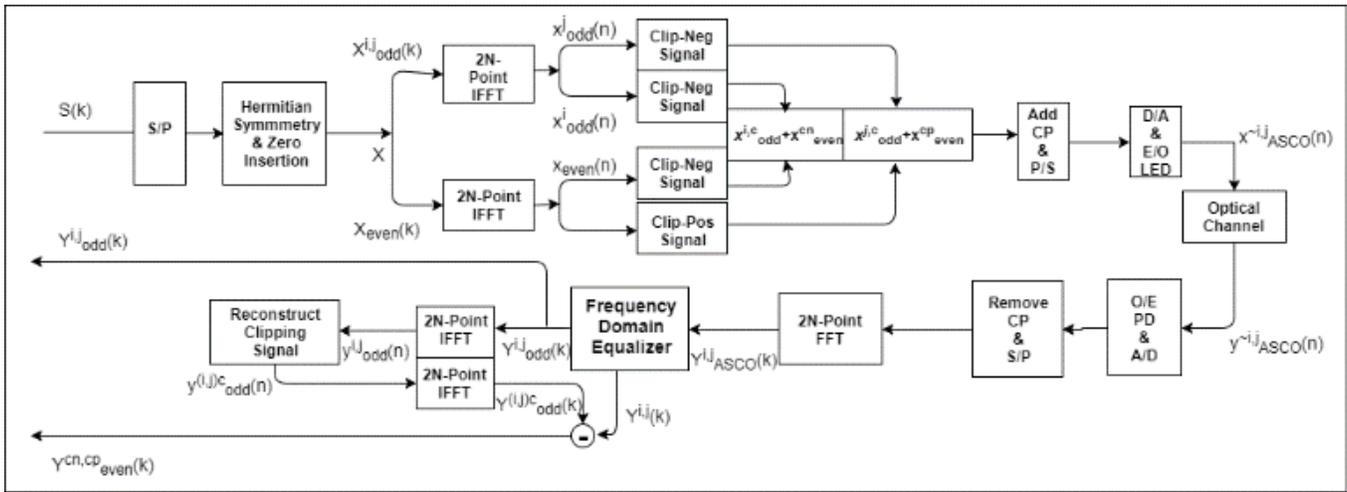


Fig. 1. Transmitter and Receiver Configuration of ASCO-OFDM

At the receiver end the channel state information (CSI) can be assumed to be well known. $Y_{ASCO}^{ij}(k)$ is operated by frequency domain equalizer, which is an output of $2N$ point FFT. By mining the odd components of Y_{odd}^{ij} , x_{odd}^{ij} can be recovered. By transforming $Y_{odd}^{ij}(k)$ into time domain, a reconstructing clipping signal block reconstruct a reference signal $y_{odd}^{(i,j)c}(k)$. Finally $Y_{even}^{cn,cp}$ is obtained by

subtracting $Y^{ij}(k)$ from the time domain version of reference signal.

B. Improved novel scheme (ASDCO)-OFDM.

The improved ASDCO-OFDM's block diagram is displayed in Fig 2. Suppose the input to the system is a set of symbols consisting of complex data given by $S = [S_0, S_1, S_2, \dots, S_{N-2}]^T$. Quadrature amplitude modulation technique is used to

modulate these complex data symbols using combination of 4QAM, 16QAM or 64QAM. Since a novel transmission scheme is utilized by improved ASCO-OFDM framework. The input to the system is a block which is separated into 3 parts out of which two of the signal vectors are of lengths $(N/2) \times 1$ and $(N/2 - 1) \times 1$ respectively, thus total number of complex data symbols are of length $(3N/2 - 1) \times 1$. Likewise, we have to form the IFFTs input to satisfy the Hermitian symmetry to get a real signal given by:

$$X_H = [0, S_0, S_1, \dots, S_{N/2}, 0, S_{N/2}, \dots, S_1, S_0]^T \quad (5)$$

After performing the Hermitian Symmetry and Zero Insertion operation, we introduce a block which calculates the meandc-bias of the signal X_H given by $X_{DC-bias}$ and then we subtract $X_{DC-bias}$ from X_H to yield X , this block nullifies the dc bias of subcarriers generated after the Hermitian Symmetry given by:

$$X = X_H - X_{DC-bias} \quad (6)$$

To form X_{odd}^i and X_{odd}^j signal vectors of length $2N \times 1$, two signal vectors of length $(N/2 \times 1)$ are united with signal vectors which are conjugate to them in series and in the even subcarriers we inject some zeroes, which are given by:

$$X_{odd}^i = [0, S_0^i, 0, S_1^i, 0, \dots, 0, S_{N/2}^i, 0, S_{N/2}^{i*}, 0, \dots, S_1^{i*}, 0, S_0^{i*}]^T \quad (7)$$

$$X_{odd}^j = [0, S_0^j, 0, S_0^j, 0, \dots, 0, S_{N/2}^j, 0, S_{N/2}^{j*}, 0, \dots, S_1^{j*}, 0, S_0^j]^T \quad (8)$$

The X_{even} signal vector of length $(N/2 - 1) \times 1$ is characterized correspondingly with zeroes embedded in subcarriers that are odd to frame the signal in this way:

$$X_{even} = \begin{bmatrix} 0, 0, S_0, 0, S_1, \dots, S_{N/2-1}, 0, 0, 0, S_{N/2-1}, \\ \dots, S_1, 0, S_0, 0 \end{bmatrix}^T \quad (9)$$

The Hermitian symmetry constraint is applied to each of the three signal vectors X_{even} , X_{odd}^j , X_{odd}^i . $2N$ -point IFFT operation must be performed to provide signal vectors x_{even} , x_{odd}^i and x_{odd}^j which are bipolar and real. Zero clipping operation is performed for all the non-positive values in x_{odd}^j and x_{odd}^i to produce $x_{odd}^{j,c}$ and $x_{odd}^{i,c}$ to confirm the positive prerequisite of the transmitted signal given by:

$$x_{odd}^{j,c} = 0.5(|x_{odd}^j| + x_{odd}^j) \quad (10)$$

$$x_{odd}^{i,c} = 0.5(|x_{odd}^i| + x_{odd}^i) \quad (11)$$

The relation of $x_{even}(n) = x_{even}(n + N)$ is formed, as each specimen in x_{even} is changed over from even subcarriers. Half of the data conveyed in x_{even} is lost, by clipping the non-positive values. In this manner, for transferring the data in x_{even} two signal vectors are produced x_{even}^{cp} and x_{even}^{cn} . Every negative estimation of x_{even} are cut to zero is represented by x_{even}^{cn} . Every single positive estimation of X_{even} are cut to zero represented by x_{even}^{cp} and the left over values which are less than zero are swung to positive. They are correspondingly given by:

$$x_{even}^{cn} = 0.5(|x_{even}| - x_{even}) \quad (12)$$

$$x_{even}^{cp} = 0.5(|x_{even}| + x_{even}) \quad (13)$$

At that point, we build a signal to convey the information which comprises of sequential sub-blocks, x_{ASDCO}^i and x_{ASDCO}^j which are given by:

$$x_{ASDCO}^i = x_{even}^{cn} + x_{odd}^{i,c} = 0.5(|x_{odd}^i| + x_{odd}^i + |x_{even}| + x_{even}) \quad (14)$$

$$x_{ASDCO}^j = x_{even}^{cp} + x_{odd}^{j,c} = 0.5(|x_{odd}^j| + x_{odd}^j + |x_{even}| - x_{even}) \quad (15)$$

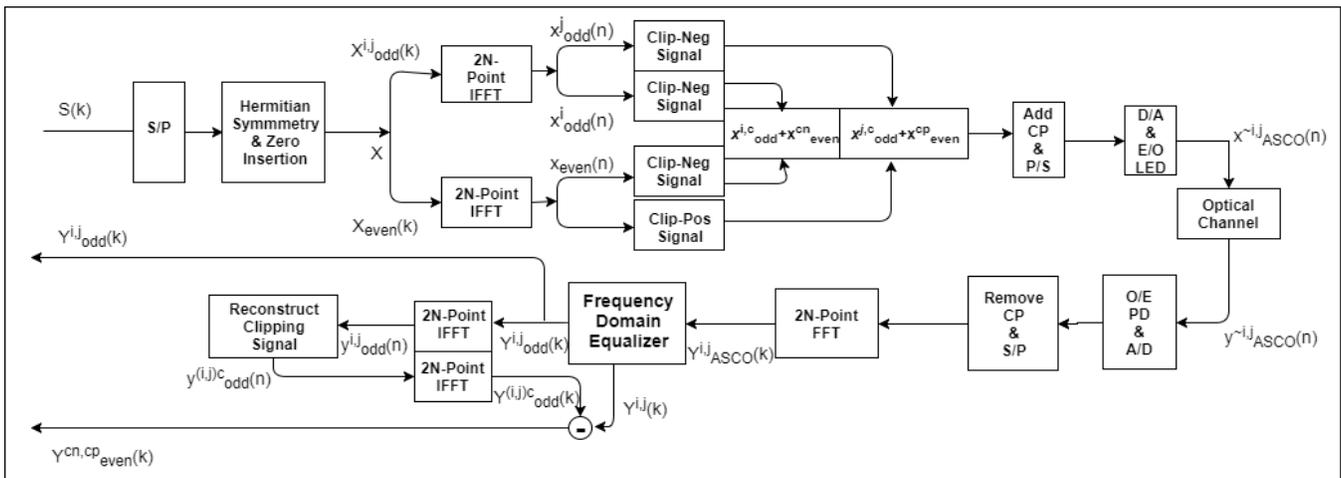


Fig. 2. Transmitter and Receiver Configuration of ASDCO-OFDM

When a cyclic prefix is attached to the transmitted signals, x_{ASDCO}^j and x_{ASDCO}^i they are signified by x_{ASDCO}^j and x_{ASDCO}^i . LED is used to convey these signal via an optical channel. The signals at the receiving end are as follows:

$$y_{ASDCO}^j(n) = w^j(n) + h(n) \otimes x_{ASDCO}^j(n) \quad (16)$$

$$y_{ASDCO}^i(n) = w^i(n) + h(n) \otimes x_{ASDCO}^i(n) \quad (17)$$

where $h(n)$ is optical channels impulse response, and additive white Gaussian noise can be represented by $w^i(n)$ or $w^j(n)$, which is the sum of all noise. The received signal y_{ASDCO}^j and y_{ASDCO}^i are one-to-one transmuted using 2N-point FFT operation to produce Y_{ASDCO}^j and Y_{ASDCO}^i into the frequency domain, after the removal of cyclic prefix. At that point, with the understanding of channel state information a zero forcing equalizer is applied Y_{ASDCO}^j and Y_{ASDCO}^i to produce:

$$Y^i = \Lambda^H Y_{ASDCO}^i \left(\Lambda^H \Lambda + \left(\frac{\alpha}{SNR} \right) I_{2N} \right)^{-1} \quad (18)$$

$$Y^j = \Lambda^H Y_{ASDCO}^j \left(\Lambda^H \Lambda + \left(\frac{\alpha}{SNR} \right) I_{2N} \right)^{-1} \quad (19)$$

Since, $\alpha = 0$ for zero forcing equalizer:

$$Y^i = Y_{ASDCO}^i / \Lambda \quad (20)$$

$$Y^j = Y_{ASDCO}^j / \Lambda \quad (21)$$

where $2N \times 2N$ diagonal matrix is represented by Λ and its diagonal is $h(n)$'s 2N-point FFT, and the Hermitian symmetry vector of Λ is given by Λ^H . Y^i and Y^j can likewise appear in the frequency domain given by:

$$Y^i = X_{even}^{cn} + X_{odd}^{i,c} = 0.5(|X_{odd}^i| + X_{odd}^i + |X_{even}^i| + X_{even}^i) \quad (22)$$

$$Y^j = X_{even}^{cp} + X_{odd}^{j,c} = 0.5(|X_{odd}^j| + X_{odd}^j + |X_{even}^j| - X_{even}^j) \quad (23)$$

If we take the 2N-point FFT of x_{odd}^j and x_{odd}^i we will get X_{odd}^j and X_{odd}^i . In a similar manner the other equivalent terms in equations 14, 15, 22, 23 are defined. We must note that on the subcarriers consisting of odd components of Y^j and Y^i the symbols $0.5X_{odd}^j$ and $0.5X_{odd}^i$ falls, and on the even subcarriers of Y^j and Y^i , these additional symbols that comprises of the other terms, $0.5(X_{even}^j + |X_{odd}^j| + |X_{even}^j|)$ and $0.5(-X_{even}^j + |X_{odd}^j| + |X_{even}^j|)$ falls, correspondingly. In this way, by removing the symbols of Y_{odd}^j and Y_{odd}^i the complex symbols can be effortlessly recuperated, and they are the odd portion of Y^j and Y^i , because the even portion of Y^j and Y^i are only influenced by the clipping noise that are caused because of $x_{odd}^{j,c}$ and $x_{odd}^{i,c}$. With a specific goal to precisely gauge the clipping noise, transformation of Y_{odd}^j and Y_{odd}^i into the time domain is done to produce real bipolar signal y_{odd}^j and y_{odd}^i , correspondingly. The manner in which $x_{odd}^{j,c}$ and $x_{odd}^{i,c}$ are

created in a similar way $y_{odd}^{j,c}$ and $y_{odd}^{i,c}$ are produced, respectively, then to produce $Y_{odd}^{i,c}$ and $Y_{odd}^{j,c}$ they are changed back to frequency domain. Contrasted with Y_{odd}^i and Y_{odd}^j , $Y_{odd}^{i,c}$ and $Y_{odd}^{j,c}$ have a similar symbol on the subcarriers that are odd, however the noise due to clippings shows up on the subcarriers that are even. In this way, Y_{even}^{cn} is obtained by deducting $Y_{odd}^{i,c}$ from Y^i and Y_{even}^{cp} is obtained by subtracting $Y_{odd}^{j,c}$ from Y^j , which are as follows:

$$Y_{even}^{cn} = Y^i - Y_{odd}^{i,c} = 0.5(|X_{even}^i| + X_{even}^i) \quad (24)$$

$$Y_{even}^{cp} = Y^j - Y_{odd}^{j,c} = 0.5(|X_{even}^j| - X_{even}^j) \quad (25)$$

We take note of that $x_{even} = x_{even}^{cn} - x_{even}^{cp}$; subsequently, Y_{even} can be assessed as follows:

$$Y_{even} = Y_{even}^{cn} - Y_{even}^{cp} \quad (26)$$

III. ANALYSIS OF THE SIGNAL FOR ASCO-OFDM AND MODIFIED ASDCO-OFDM

Under this segment, we initially examine the average Bitrate/Normalized Bandwidths of modified ASDCO-OFDM and ASCO-OFDM. We can acquire the power (optical) per bit for both systems through figuring the data bit and the transmitted signal's overall optical power.

A. Analyzing the average Bitrate/Normalized Bandwidths

Complex symbols of length $2N - 2$ are modulated for both ASCO-OFDM and modified ASDCO-OFDM while the length of the spectrum is $2N$; subsequently, for both the scheme $N/(N - 1)$ represent the normalized bandwidth. For ASCO-OFDM and modified ASDCO-OFDM, all data conveyed is isolated into two continuous sub-blocks $x_{ASCO/ASDCO}^i$ and $x_{ASCO/ASDCO}^j$, for the even subcarriers. In this way, the data x_{even} is conveyed by the even elements is reduced to half, i.e. $x_{ASCO/ASDCO}^i$ and $x_{ASCO/ASDCO}^j$ of one sub-block. As a result, for both ASCO-OFDM and modified ASDCO-OFDM, for one sub-block the average bit rate can be achieved by:

$$R_{b,ASDCO-OFDM} = (0.5 \log_2 C_{SCO} + \log_2 C_{ACO})/2 \quad (27)$$

and $((0.5 \log_2 C_{SCO} + \log_2 C_{ACO})/2)/(N/(N - 1))$ represent the normal bit rate/normalized bandwidth, where C_{ACO} and C_{SCO} are correspondingly characterized. In ASCO-OFDM and modified ASDCO-OFDM for both even and odd subcarriers we apply different constellation, in Table I for both the modified schemes we look into the average Bitrate/Normalized Bandwidths.

TABLE I. ASDCO-OFDM AVERAGE BITRATE/NORMALIZED BANDWIDTHS WITH DIFFERENT CONSTELLATION COMBINATIONS

Symbol	ASDCO-OFDM constellation size	B.R./N. B
P	Even subcarriers 4 QAM Odd subcarriers 4 QAM	1.5

Q	Even subcarriers 4 QAM Odd subcarriers 16 QAM	2.5
R	Even subcarriers 4 QAM Odd subcarriers 64 QAM	3.5
S	Even subcarriers 16 QAM Odd subcarriers 16 QAM	3
T	Even subcarriers 16 QAM Odd subcarriers 64 QAM	4
U	Even subcarriers 64 QAM Odd subcarriers 64 QAM	4.5

B. Analyzing the Optical power/bit

So as to discover the precise $P_{opt/bit}$, for ASCO and ASDCO-OFDM, in the transmitted optical signal we add each and every value, without the addition of cyclic prefix.

Two back to back sub-blocks are present in transmitted optical signal i.e. $x_{ASCO/ASDCO}^i$ and $x_{ASCO/ASDCO}^j$, for both ASCO and ASDCO OFDM techniques. Consequently, for both the transmitted ASCO and ASDCO OFDM signal the aggregate optical power is given by:

$$P_{opt,ASDCO} = \sum_{n=0}^{2N-1} x_{ASDCO}^i(n) + x_{ASDCO}^j(n) \quad (28)$$

The input block comprising of symbols that are complex for ASDCO-OFDM of length $3N/2 - 1$ are isolated in three sections. To produce $x_{odd}^{j,c}$ and $x_{odd}^{i,c}$ modulation of complex symbols contained in two blocks of length $N/2$ are done by ACO-OFDM. To obtain x_{even}^{cn} and x_{even}^{cp} , modulation of complex symbols contained in one block of length $N/2 - 1$ is done by SCO-OFDM. Hence, for ASCO-OFDM and modified ASDCO-OFDM the total transmitted bits are given by:

$$T_{b,ASDCO-OFDM} = \left(\frac{N}{2} - 1\right) \log_2 C_{SCO} + 2 \left(\frac{N}{2}\right) \log_2 C_{ACO} \quad (29)$$

TABLE II. COMPARISON OF POWER(OPTICAL) PER BIT OF ASCO-OFDM AND ASDCO-OFDM

Constellation Size	ASCO-OFDM	ASDCO-OFDM
Odd subcarriers 4-QAM Even subcarriers 4-QAM	2.2	.66
Odd subcarriers 16-QAM Even subcarriers 4-QAM	2.1	1.511
Odd subcarriers 64-QAM Even subcarriers 4-QAM	2.5	1.8
Odd subcarriers 16-QAM Even subcarriers 16-QAM	2.4	1.531
Odd subcarriers 64-QAM Even subcarriers 16-QAM	2.7	1.642
Odd subcarriers 64-QAM Even subcarriers 64-QAM	3.2	1.611

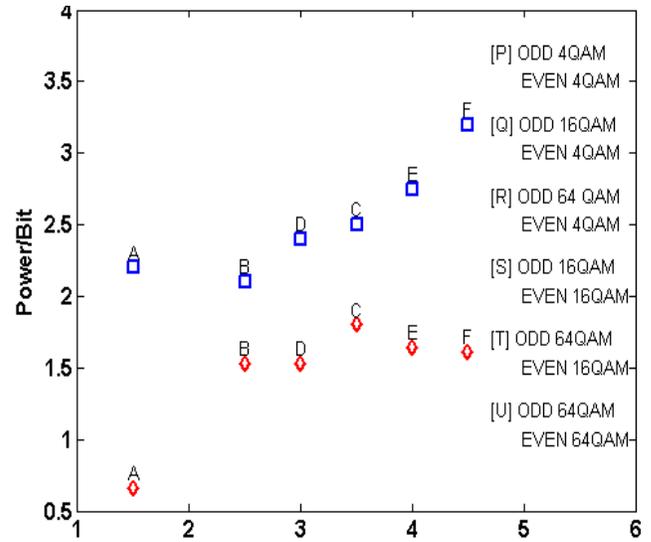


Fig. 3. Bit rate/Normalized Bandwidth versus

IV. SIMULATION RESULTS

Comparison of the outcomes of $P_{opt/bit}$ for ASCO and ASDCO OFDM are shown in Figure 3. Combination of six constellation represented by P to U, which are given in Table II. They are operated on even and odd subcarriers of two systems. ASCO-OFDM is symbolized by squares, and modified ASDCO-OFDM is symbolized by rhombus. 64 QAM symbols are symbolized by rhombus F and square F on all subcarriers for modified ASDCO-OFDM and ASCO-OFDM respectively.

On the off chance that modulation of the two frameworks are done by a similar constellation combination. Bit rate/normalized bandwidth of ASDCO-OFDM and ASCO-OFDM are comparable.

On the other hand, requirement of optical power in modified ASDCO-OFDM is less than ASCO-OFDM for each bit because of mean DC-bias subtraction from the Hermitian symmetric signal after the modulation. Despite the similarity in the Bit rate/Normalized Bandwidth of ASDCO-OFDM, the efficiency of the optical power for grouping of dissimilar constellation is more compared to that of ASCO-OFDM. As a result, in terms of optical power of ASCO-OFDM is less effective in comparison with modified ASDCO-OFDM.

The SER comparison is illustrated in Figure 4 for ASCO-OFDM and modified ASDCO-OFDM when combination of different constellations are applied to represent similar combination of constellation we use the similar marker. ASCO-OFDM is denoted by a dashed curve whereas a solid curve denotes modified ASDCO-OFDM. Likewise, some particular comparison pairs ought to be explained. Looking at the dashed triangle curve to the solid rhombus curve, 16-4 QAM ASCO-OFDM have similar symbol error rate performance as modified ASDCO-OFDM with 16-16 QAM,

and the requirement of optical power for both the combination is more or less similar as depicted in Figure 4. While accomplishing a similar Bitrate/Normalized Bandwidth, ASDCO-OFDM beats ASCO-OFDM as far as the performance of SER and efficiency of optical is concerned, which is

revealed for all constellation combination. Lastly, we bring up that modified ASDCO-OFDM (solid curve) is superior to ASCO-OFDM (dashed curve) in all view points since the performance of SER is better and the optical power per bit requirement is less.

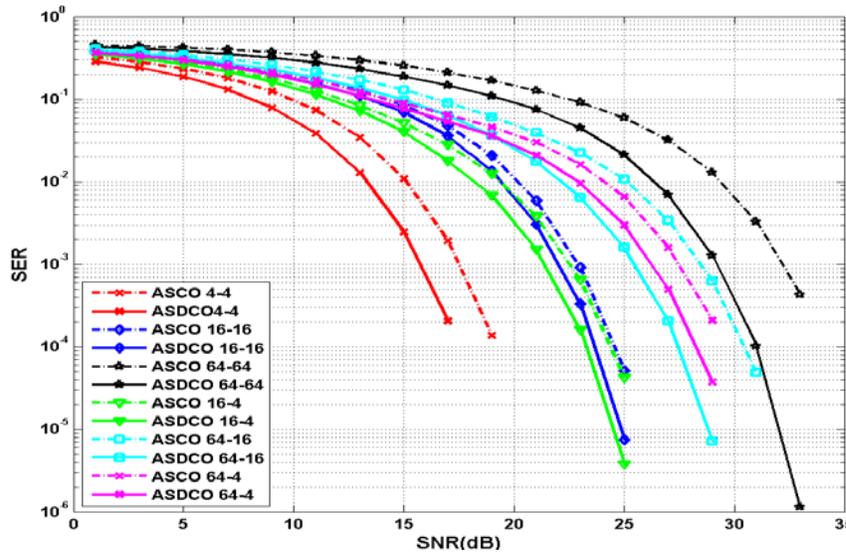


Fig. 4. Symbol error rate versus signal to noise ratio

V. CONCLUSION

In this paper, we suggest an improved methodology known as ASDCO-OFDM which can be utilized in wireless optical systems. Mean dc-bias of subcarriers is subtracted from the Hermitian symmetric signal for power efficiency. Odd subcarriers are modulated using ACO-OFDM whereas even subcarriers are modulated using SCO-OFDM which is a novel modulation scheme. To convey the symbols in case of SCO-OFDM, we efficaciously implement two successive sub-blocks on the subcarriers that are even and is deprived of DC bias. Meanwhile the even part and the odd part of two frameworks can be discretely distinguished, diverse combinations of constellation are taken into record for modulation. Contrasted with ASCO-OFDM, our modified model exhibits excellent performance in case of SER and the optical power requirement per bit is less. Thus, we can say that modified ASDCO-OFDM is an appealing decision for wireless optical system.

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